

## Gas Pipeline Flow - SI Units

American Gas Association (AGA) equation for fully turbulent isothermal gas flow  
(Reference: Eq-17-18, Section 17, GPSA Engineering Data Book, Eleventh Edition, 1998)

$$Q = 0.018 \times \frac{T_s}{P_s} \times E \times \left[ 4 \log_{10} \left( \frac{3.7d}{\epsilon} \right) \right] \times \left[ \frac{P_1^2 - P_2^2}{\gamma L_m T_{avg} Z_{avg}} \right]^{0.5} \times d^{2.5}$$

where:

- Q = flow rate of gas, m<sup>3</sup>/day at standard conditions  
 T<sub>s</sub> = Standard Temperature = 288.9 K  
 P<sub>s</sub> = Standard Pressure = 101.56 kPa (abs)  
 E = pipeline efficiency factor (fraction)  
 = 1 in the absence of field data (also for new straight pipe with no diameter change)  
 = 0.95 for very good operating conditions, typically through first 12–18 months  
 = 0.92 for average operating conditions  
 = 0.85 for unfavourable operating conditions  
 d = internal diameter of pipe, mm  
 ε = pipe material absolute roughness, mm (commonly used value for bare steel pipe = 0.046)  
 P<sub>1</sub> = Inlet or Start Pressure, kPa (abs)  
 P<sub>2</sub> = Outlet or End Pressure, kPa (abs)  
 γ = relative density of flowing gas (air = 1.0), dimensionless  
 Can be calculated as follows:

$$\gamma = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

- L<sub>m</sub> = length of pipeline, m  
 T<sub>avg</sub> = average temperature, K

$$T_{avg} = \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} + T_{soil}$$

- T<sub>in</sub> = Gas temperature at inlet, K  
 T<sub>out</sub> = Gas temperature at outlet, K  
 T<sub>soil</sub> = Soil temperature, K

- Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \left( \frac{P_{avg} \times 5270 \times 10^{1.785\gamma}}{T_{avg}^{3.825}} \right) \right]^2}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

### Inputs

$T_s =$	288.9	K
$P_s =$	101.56	kPa (abs)
$E =$	0.92	dimensionless
$d =$	489	mm
$\varepsilon =$	0.046	mm (standard value for bare CS pipe)
$P_1 =$	7,000	kPa (abs)
$P_2 =$	5,600	kPa (abs)
$L_m =$	16,000	m
$MW =$	17.38	kg/kg-mol
$T_{in} =$	30	°C
$T_{out} =$	27	°C
$T_{soil} =$	18	°C

### Calculations

$\gamma =$	0.6	dimensionless
$T_{in} =$	303.15	K
$T_{out} =$	300.15	K
$T_{soil} =$	291.15	K
$T_{avg} =$	301.58	K
$P_{avg} =$	6,325.9	kPa (abs)
$Z_{avg} =$	0.78	dimensionless
$Q =$	12,756,926	m <sup>3</sup> /day @std. conditions of 101.56 kPa(abs) & 15.75°C
	531,538.6	m <sup>3</sup> /h @std. conditions of 101.56 kPa(abs) & 15.75°C

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## Gas Pipeline Flow - U.S. Customary Units

American Gas Association (AGA) equation for fully turbulent isothermal gas flow  
(Reference: Eq-17-18, Section 17, GPSA Engineering Data Book, Twelfth Edition-FPS, 2)

$$Q = 38.77 \times \frac{T_b}{P_b} \times E \times \left[ 4 \log_{10} \left( \frac{3.7D}{\varepsilon} \right) \right] \times \left[ \frac{P_1^2 - P_2^2}{SL_m T_{avg} Z_{avg}} \right]^{0.5} \times d^{2.5}$$

where:

- Q = flow rate of gas, ft<sup>3</sup>/day at base conditions  
 T<sub>b</sub> = Base Temperature = 520 R  
 P<sub>b</sub> = Base Pressure = 14.73 psia  
 E = pipeline efficiency factor (fraction)  
 = 1 in the absence of field data (also for new straight pipe with no diameter change)  
 = 0.95 for very good operating conditions, typically through first 12–18 months  
 = 0.92 for average operating conditions  
 = 0.85 for unfavourable operating conditions  
 d = internal diameter of pipe, inch  
 D = internal diameter of pipe, ft  
 ε = pipe material absolute roughness, ft (commonly used value for bare steel pipe = 0.0001)  
 P<sub>1</sub> = Inlet or Start Pressure, psia  
 P<sub>2</sub> = Outlet or End Pressure, psia  
 S = specific gravity of flowing gas (air = 1.0), dimensionless  
 Can be calculated as follows:

$$S = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

- L<sub>m</sub> = length of pipeline, miles  
 T<sub>avg</sub> = average temperature, R

$$T_{avg} = \left[ \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} \right] + T_{soil}$$

- T<sub>in</sub> = Gas temperature at inlet, R  
 T<sub>out</sub> = Gas temperature at outlet, R  
 T<sub>soil</sub> = Soil temperature, R

- Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \frac{(P_{avg} + 14.7) \times 344400 \times 10^{1.7855}}{T_{avg}^{3.825}} \right]}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

### Inputs

$T_b =$	520	R	
$P_b =$	14.73	psia	
$E =$	0.92	dimensionless	
$d =$	19.25	inch	
$\varepsilon =$	0.00015	ft	(standard value for bare CS pipe)
$P_1 =$	1,015	psia	
$P_2 =$	812	psia	
$L_m =$	10	miles	
$MW =$	17.38	lb/lb-mol	
$T_{in} =$	86	°F	
$T_{out} =$	81	°F	
$T_{soil} =$	64	°F	

### Calculations

$S =$	0.6	dimensionless	
$T_{in} =$	546	R	
$T_{out} =$	541	R	
$T_{soil} =$	524	R	
$T_{avg} =$	543.39	R	
$P_{avg} =$	917.3	psia	
$D =$	1.6	ft	
$Z_{avg} =$	0.88	dimensionless	
$Q =$	426,925,291	ft <sup>3</sup> /day	@base conditions of 14.73 psia & 60°F
	296,475.9	ft <sup>3</sup> /min	@base conditions of 14.73 psia & 60°F

## Gas Pipeline Flow - SI Units

### Weymouth equation for fully turbulent isothermal gas flow

(Reference: Equation 2.32, Gas Pipeline Hydraulics by E. Shashi Menon)

$$Q = 0.0037435 \times \frac{T_s}{P_s} \times E \times \left[ \frac{P_1^2 - P_2^2}{\gamma L_m T_{avg} Z_{avg}} \right]^{0.5} \times d^{2.667}$$

where:

Q = flow rate of gas, m<sup>3</sup>/day at standard conditions

T<sub>s</sub> = Standard Temperature =

288.9 K

P<sub>s</sub> = Standard Pressure =

101.56 kPa (abs)

d = internal diameter of pipe, mm

P<sub>1</sub> = Inlet or Start Pressure, kPa (abs)

P<sub>2</sub> = Outlet or End Pressure, kPa (abs)

γ = relative density of flowing gas (air = 1.0), dimensionless

Can be calculated as follows:

$$\gamma = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

L<sub>m</sub> = length of pipeline, km

T<sub>avg</sub> = average temperature, K

$$T_{avg} = \left[ \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} \right] + T_{soil}$$

T<sub>in</sub> = Gas temperature at inlet, K

T<sub>out</sub> = Gas temperature at outlet, K

T<sub>soil</sub> = Soil temperature, K

Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \left( \frac{P_{avg} \times 5270 \times 10^{1.785\gamma}}{T_{avg}^{3.825}} \right) \right]^2}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

#### Notes:

1. Weymouth equation is recommended to be used for short pipelines & gathering stations.

**Inputs**

$T_s =$	288.9	K
$P_s =$	101.56	kPa (abs)
$E =$	0.92	dimensionless
$d =$	489	mm
$P_1 =$	7,000	kPa (abs)
$P_2 =$	5,600	kPa (abs)
$L_m =$	16	km
$MW =$	17.38	kg/kg-mol
$T_{in} =$	30	°C
$T_{out} =$	27	°C
$T_{soil} =$	18	°C

**Calculations**

$\gamma =$	0.6	dimensionless
$T_{in} =$	303.15	K
$T_{out} =$	300.15	K
$T_{soil} =$	291.15	K
$T_{avg} =$	301.58	K
$P_{avg} =$	6,325.9	kPa (abs)
$Z_{avg} =$	0.78	dimensionless
$Q =$	12,839,373	$m^3/day$ @std. conditions of 101.56 kPa(abs) & 15.75°C
	534,973.9	$m^3/h$ @std. conditions of 101.56 kPa(abs) & 15.75°C

**Observation:**

For the same conditions inlet & outlet pressure, line size, line length, efficiency factor E & avg. gas flowing temperature, Weymouth equation gives **closer approximation** of flow to the AGA equation compared to the Panhandle A & B equation.

## Gas Pipeline Flow - U.S. Customary Units

### Weymouth equation for fully turbulent isothermal gas flow

(Reference: Equation 2.30, Gas Pipeline Hydraulics by E. Shashi Menon)

$$Q = 433.5 \times \frac{T_b}{P_b} \times E \times \left[ \frac{P_1^2 - P_2^2}{SL_m T_{avg} Z_{avg}} \right]^{0.5} \times d^{2.667}$$

where:

- Q = flow rate of gas, ft<sup>3</sup>/day at base conditions  
 T<sub>b</sub> = Base Temperature = 520 R  
 P<sub>b</sub> = Base Pressure = 14.73 psia  
 d = internal diameter of pipe, inch  
 P<sub>1</sub> = Inlet or Start Pressure, psia  
 P<sub>2</sub> = Outlet or End Pressure, psia  
 S = specific gravity of flowing gas (air = 1.0), dimensionless

Can be calculated as follows:

$$S = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

L<sub>m</sub> = length of pipeline, miles

T<sub>avg</sub> = average temperature, R

$$T_{avg} = \left[ \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} \right] + T_{soil}$$

T<sub>in</sub> = Gas temperature at inlet, R

T<sub>out</sub> = Gas temperature at outlet, R

T<sub>soil</sub> = Soil temperature, R

Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \frac{(P_{avg} + 14.7) \times 344400 \times 10^{1.7855}}{T_{avg}^{3.825}} \right]}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

#### Notes:

1. Weymouth equation is recommended to be used for short pipelines & gathering stations.

**Inputs**

$T_b =$	520	R
$P_b =$	14.73	psia
$E =$	0.92	dimensionless
$d =$	19.25	inch
$P_1 =$	1,015	psia
$P_2 =$	812	psia
$L_m =$	10	miles
$MW =$	17.38	lb/lb-mol
$T_{in} =$	86	°F
$T_{out} =$	81	°F
$T_{soil} =$	64	°F

**Calculations**

$S =$	0.6	dimensionless
$T_{in} =$	546	R
$T_{out} =$	541	R
$T_{soil} =$	524	R
$T_{avg} =$	543.39	R
$P_{avg} =$	917.3	psia
$Z_{avg} =$	0.88	dimensionless
$Q =$	425,379,559	ft <sup>3</sup> /day @base conditions of 14.73 psia & 60°F
	295,402.5	ft <sup>3</sup> /min @base conditions of 14.73 psia & 60°F

**Observation:**

For the same conditions inlet & outlet pressure, line size, line length, efficiency factor E & avg. gas flowing temperature, Weymouth equation gives **closer approximation** of flow to the AGA equation compared to the Panhandle A & B equation.

## Gas Pipeline Flow - SI Units

### Panhandle A equation for partially turbulent isothermal gas flow

(Reference: Equation 2.35, Gas Pipeline Hydraulics by E. Shashi Menon)

$$0.0045965 \times \left(\frac{T_s}{P_s}\right)^{1.0788} \times E \times \left[\frac{P_1^2 - P_2^2}{\gamma^{0.8539} L_m T_{avg} Z_{avg}}\right]^{0.5394} \times d^{2.6182}$$

where:

- Q = flow rate of gas, m<sup>3</sup>/day at standard conditions  
 T<sub>s</sub> = Standard Temperature = 288.9 K  
 P<sub>s</sub> = Standard Pressure = 101.56 kPa (abs)  
 E = pipeline efficiency factor (fraction)  
 = 1 in the absence of field data (also for new straight pipe with no diameter changes)  
 = 0.95 for very good operating conditions, typically through first 12–18 months  
 = 0.92 for average operating conditions  
 = 0.85 for unfavourable operating conditions  
 d = internal diameter of pipe, mm  
 P<sub>1</sub> = Inlet or Start Pressure, kPa (abs)  
 P<sub>2</sub> = Outlet or End Pressure, kPa (abs)  
 γ = relative density of flowing gas (air = 1.0), dimensionless

Can be calculated as follows:

$$\gamma = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

L<sub>m</sub> = length of pipeline, km

T<sub>avg</sub> = average temperature, K

$$T_{avg} = \frac{T_{in} - T_{out}}{\ln\left(\frac{T_{in} - T_{soil}}{T_{out} - T_{soil}}\right)} + T_{soil}$$

T<sub>in</sub> = Gas temperature at inlet, K

T<sub>out</sub> = Gas temperature at outlet, K

T<sub>soil</sub> = Soil temperature, K

Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[1 + \left(\frac{P_{avg} \times 5270 \times 10^{1.785\gamma}}{T_{avg}^{3.825}}\right)\right]^2}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

$$Re = 0.5134 \times \frac{P_s}{T_s} \times \left( \frac{\gamma \times Q}{\mu_{avg} \times d} \right)$$

where:

Re = Reynolds no.

μ<sub>avg</sub> = avg. viscosity of gas, Poise (From "Gas Viscosity Panhandle A" sheet)

**Notes:**

1. Panhandle A equation should be used for large diameter (≥250 mm) pipelines & for long distance pipelines.
2. Efficiency factor of E = 0.92 is recommended for use with the Panhandle A equation.
3. Panhandle A eqn gives reasonable flow rates (low errors) if Reynolds no. is between 5 & 11 million

**Inputs**

$T_s =$	288.9	K
$P_s =$	101.56	kPa (abs)
$E =$	0.92	dimensionless
$d =$	489	mm
$P_1 =$	7,000	kPa (abs)
$P_2 =$	5,600	kPa (abs)
$L_m =$	16	km
$MW =$	17.38	kg/kg-mol
$T_{in} =$	30	°C
$T_{out} =$	27	°C
$T_{soil} =$	18	°C
$\mu_{avg} =$	0.000127	P

**Calculations**

$\gamma =$	0.6	dimensionless
$T_{in} =$	303.15	K
$T_{out} =$	300.15	K
$T_{soil} =$	291.15	K
$T_{avg} =$	301.58	K
$P_{avg} =$	6,325.9	kPa (abs)
$Z_{avg} =$	0.78	dimensionless
$Q =$	17,298,972	m <sup>3</sup> /day @std. conditions of 101.56 kPa(abs) & 15.75°C
	720,790.5	m <sup>3</sup> /h @std. conditions of 101.56 kPa(abs) & 15.75°C
$Re =$	30,211,495	dimensionless
	FLOW ERROR HIGH	

**Observation:**

For the same conditions inlet & outlet pressure, line size, line length, efficiency factor E & avg. gas flowing temperature, Panhandle A equation gives **much higher** flow than AGA & Weymouth equation.

## Gas Pipeline Flow - U.S. Customary Units

Panhandle A equation for partially turbulent isothermal gas flow  
(Reference: Equation 2.35, Gas Pipeline Hydraulics by E. Shashi Menon)

$$435.87 \times \left( \frac{T_b}{P_b} \right)^{1.0788} \times E \times \left[ \frac{P_1^2 - P_2^2}{S^{0.8539} L_m T_{avg} Z_{avg}} \right]^{0.5394} \times d^{2.6182}$$

where:

- Q = flow rate of gas, ft<sup>3</sup>/day at base conditions  
 T<sub>b</sub> = Base Temperature = 520 R  
 P<sub>b</sub> = Base Pressure = 14.73 psia  
 E = pipeline efficiency factor (fraction)  
 = 1 in the absence of field data (also for new straight pipe with no diameter changes)  
 = 0.95 for very good operating conditions, typically through first 12–18 months  
 = 0.92 for average operating conditions  
 = 0.85 for unfavourable operating conditions  
 d = internal diameter of pipe, inch  
 P<sub>1</sub> = Inlet or Start Pressure, psia  
 P<sub>2</sub> = Outlet or End Pressure, psia  
 S = specific gravity of flowing gas (air = 1.0), dimensionless  
 Can be calculated as follows:

$$S = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

L<sub>m</sub> = length of pipeline, miles

T<sub>avg</sub> = average temperature, R

$$T_{avg} = \left[ \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} \right] + T_{soil}$$

T<sub>in</sub> = Gas temperature at inlet, R

T<sub>out</sub> = Gas temperature at outlet, R

T<sub>soil</sub> = Soil temperature, R

Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \frac{(P_{avg} + 14.7) \times 344400 \times 10^{1.7855}}{T_{avg}^{3.825}} \right]}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

$$Re = 0.0004778 \times \frac{P_b}{T_b} \times \left( \frac{S \times Q}{\mu_{avg} \times d} \right)$$

where:

Re = Reynolds no.

μ<sub>avg</sub> = avg. viscosity of gas, lb/ft.s (From "Gas Viscosity Panhandle A" sheet)

Notes:

1. Panhandle A equation should be used for large diameter (≥250 mm) pipelines & for long distance pipelines.
2. Efficiency factor of E = 0.92 is recommended for use with the Panhandle A equation.
3. Panhandle A eqn gives reasonable flow rates (low errors) if Reynolds no. is between 5 & 11 million

### Inputs

$T_b =$	520	R
$P_b =$	14.73	psia
$E =$	0.92	dimensionless
$d =$	19.25	inch
$P_1 =$	1,015	psia
$P_2 =$	812	psia
$L_m =$	10	miles
$MW =$	17.38	lb/lb-mol
$T_{in} =$	86	°F
$T_{out} =$	81	°F
$T_{soil} =$	64	°F
$\mu_{avg} =$	0.000008	lb/ft.s

### Calculations

$S =$	0.6	dimensionless
$T_{in} =$	546	R
$T_{out} =$	541	R
$T_{soil} =$	524	R
$T_{avg} =$	543.39	R
$P_{avg} =$	917.3	psia
$Z_{avg} =$	0.88	dimensionless
$Q =$	570,232,691	ft <sup>3</sup> /day @base conditions of 14.73 psia & 60°F
	395,994.9	ft <sup>3</sup> /min @base conditions of 14.73 psia & 60°F
$Re =$	28,740,594	dimensionless
	FLOW ERROR HIGH	

### Observation:

For the same conditions inlet & outlet pressure, line size, line length, efficiency factor E & avg. gas flowing temperature, Panhandle A equation gives **much higher** flow than AGA & Weymouth equation.

## Gas Pipeline Flow - SI Units

### Panhandle B equation for fully turbulent isothermal gas flow

(Reference: Equation 2.37, Gas Pipeline Hydraulics by E. Shashi Menon)

$$0.01002 \times \left( \frac{T_s}{P_s} \right)^{1.02} \times E \times \left[ \frac{P_1^2 - P_2^2}{\gamma^{0.961} L_m T_{avg} Z_{avg}} \right]^{0.51} \times d^{2.53}$$

where:

- Q = flow rate of gas, m<sup>3</sup>/day at standard conditions  
 T<sub>s</sub> = Standard Temperature = 288.9 K  
 P<sub>s</sub> = Standard Pressure = 101.56 kPa (abs)  
 E = pipeline efficiency factor (fraction)  
 = 1 in the absence of field data (also for new straight pipe with no diameter changes)  
 = 0.95 for very good operating conditions, typically through first 12–18 months  
 = 0.92 for average operating conditions  
 = 0.85 for unfavourable operating conditions  
 d = internal diameter of pipe, mm  
 P<sub>1</sub> = Inlet or Start Pressure, kPa (abs)  
 P<sub>2</sub> = Outlet or End Pressure, kPa (abs)  
 γ = relative density of flowing gas (air = 1.0), dimensionless

Can be calculated as follows:

$$\gamma = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

L<sub>m</sub> = length of pipeline, km

T<sub>avg</sub> = average temperature, K

$$T_{avg} = \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} + T_{soil}$$

T<sub>in</sub> = Gas temperature at inlet, K

T<sub>out</sub> = Gas temperature at outlet, K

T<sub>soil</sub> = Soil temperature, K

Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \left( \frac{P_{avg} \times 5270 \times 10^{1.785\gamma}}{T_{avg}^{3.825}} \right) \right]^2}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

$$Re = 0.5134 \times \frac{P_s}{T_s} \times \left( \frac{\gamma \times Q}{\mu_{avg} \times d} \right)$$

where:

Re = Reynolds no.

μ<sub>avg</sub> = avg. viscosity of gas, Poise (From "Gas Viscosity Panhandle B" sheet)

**Notes:**

1. Panhandle B equation should be used for large diameter (≥250 mm) pipelines & for long distance pipelines.
2. Efficiency factor varies between about 0.88 & 0.94 for use with the Panhandle B equation.
3. Panhandle B equation is found to be fairly accurate in turbulent flow for Reynolds numbers between 4 to 40 million.

**Inputs**

$T_s =$	288.9	K
$P_s =$	101.56	kPa (abs)
$E =$	0.92	dimensionless
$d =$	489	mm
$P_1 =$	7,000	kPa (abs)
$P_2 =$	5,600	kPa (abs)
$L_m =$	16	km
$MW =$	17.38	kg/kg-mol
$T_{in} =$	30	°C
$T_{out} =$	27	°C
$T_{soil} =$	18	°C
$\mu_{avg} =$	0.000127	P

**Calculations**

$\gamma =$	0.6	dimensionless
$T_{in} =$	303.15	K
$T_{out} =$	300.15	K
$T_{soil} =$	291.15	K
$T_{avg} =$	301.58	K
$P_{avg} =$	6,325.9	kPa (abs)
$Z_{avg} =$	0.78	dimensionless
$Q =$	16,265,509	m <sup>3</sup> /day @std. conditions of 101.56 kPa(abs) & 15.75°C
	677,729.5	m <sup>3</sup> /h @std. conditions of 101.56 kPa(abs) & 15.75°C
$Re =$	28,406,621	dimensionless
	FLOW ERROR LOW	

**Observation:**

For the same conditions inlet & outlet pressure, line size, line length, efficiency factor E & avg. gas flowing temperature, Panhandle B equation gives **lower** flow than Panhandle A equation.

## Gas Pipeline Flow - U.S. Customary Units

### Panhandle B equation for fully turbulent isothermal gas flow

(Reference: Equation 2.36, Gas Pipeline Hydraulics by E. Shashi Menon)

$$737 \times \left( \frac{T_b}{P_b} \right)^{1.02} \times E \times \left[ \frac{P_1^2 - P_2^2}{S^{0.961} L_m T_{avg} Z_{avg}} \right]^{0.51} \times d^{2.53}$$

where:

- Q = flow rate of gas, ft<sup>3</sup>/day at base conditions  
 T<sub>b</sub> = Base Temperature = 520 R  
 P<sub>b</sub> = Base Pressure = 14.73 psia  
 E = pipeline efficiency factor (fraction)  
 = 1 in the absence of field data (also for new straight pipe with no diameter changes)  
 = 0.95 for very good operating conditions, typically through first 12–18 months  
 = 0.92 for average operating conditions  
 = 0.85 for unfavourable operating conditions  
 d = internal diameter of pipe, inch  
 P<sub>1</sub> = Inlet or Start Pressure, psia  
 P<sub>2</sub> = Outlet or End Pressure, psia  
 S = specific gravity of flowing gas (air = 1.0), dimensionless  
 Can be calculated as follows:

$$S = \frac{MW}{28.96}$$

where MW = molecular weight of the gas under consideration

L<sub>m</sub> = length of pipeline, miles

T<sub>avg</sub> = average temperature, R

$$T_{avg} = \left[ \frac{T_{in} - T_{out}}{\ln \left( \frac{T_{in} - T_{soil}}{T_{out} - T_{soil}} \right)} \right] + T_{soil}$$

T<sub>in</sub> = Gas temperature at inlet, R

T<sub>out</sub> = Gas temperature at outlet, R

T<sub>soil</sub> = Soil temperature, R

Z<sub>avg</sub> = average compressibility factor, dimensionless

$$Z_{avg} = \frac{1}{\left[ 1 + \frac{(P_{avg} + 14.7) \times 344400 \times 10^{1.785S}}{T_{avg}^{3.825}} \right]}$$

$$P_{avg} = \frac{2}{3} \left[ P_1 + P_2 - \frac{P_1 P_2}{P_1 + P_2} \right]$$

$$Re = 0.0004778 \times \frac{P_b}{T_b} \times \left( \frac{S \times Q}{\mu_{avg} \times d} \right)$$

where:

- Re = Reynolds no.  
 μ<sub>avg</sub> = avg. viscosity of gas, lb/ft.s (From "Gas Viscosity Panhandle B" sheet)

#### Notes:

1. Panhandle B equation should be used for large diameter (≥10 inch) pipelines & for long distance pipelines.
2. Efficiency factor varies between about 0.88 & 0.94 for use with the Panhandle B equation.
3. Panhandle B equation is found to be fairly accurate in turbulent flow for Reynolds numbers between 4 to 40 million.

**Inputs**

$T_b =$	520	R
$P_b =$	14.73	psia
$E =$	0.92	dimensionless
$d =$	19.25	inch
$P_1 =$	1,015	psia
$P_2 =$	812	psia
$L_m =$	10	miles
$MW =$	17.38	lb/lb-mol
$T_{in} =$	86	°F
$T_{out} =$	81	°F
$T_{soil} =$	64	°F
$\mu_{avg} =$	0.000008	lb/ft.s

**Calculations**

$S =$	0.6	dimensionless
$T_{in} =$	546	R
$T_{out} =$	541	R
$T_{soil} =$	524	R
$T_{avg} =$	543.39	R
$P_{avg} =$	917.3	psia
$Z_{avg} =$	0.88	dimensionless
$Q =$	538,175,445	ft <sup>3</sup> /day @base conditions of 14.73 psia & 60°F
	373,732.9	ft <sup>3</sup> /min @base conditions of 14.73 psia & 60°F
$Re =$	27,124,860	dimensionless
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**Observation:**

For the same conditions inlet & outlet pressure, line size, line length, efficiency factor E & avg. gas flowing temperature, Panhandle B equation gives **lower** flow than Panhandle A equation.

**Gas Viscosity Correlation (Lee, Gonzalez & Eakin)(For "Panhandle A Eqn US" worksheet)**

$$\mu_{avg} = K \times \exp(X \times \rho_{avg}^Y)$$

where:

$\mu_{avg}$  = average gas viscosity, cP

$\rho_{avg}$  = average gas density, g/ml

$$K = \frac{0.0001 \times (7.77 + 0.0063 MW) \times T_{avgR}^{1.5}}{122.4 + 12.9MW + T_{avgR}}$$

where:

MW = molecular weight of the gas

$T_{avgR}$  = Avg. temperature of the gas in R

$$X = 2.57 + \frac{19145}{T_{avgR}} + 0.0095MW$$

$$Y = 1.11 + 0.04X$$

$$\rho_{avg} = \frac{P_{avg} \times MW}{R \times T_{avg} \times Z_{avg} \times 1000}$$

where:

R = 8.314 kPaa\*m<sup>3</sup>/kmol-K

$P_{avg}$  = Avg. Pressure of gas, kPa(abs) (from "Panhandle A Eqn US"sheet)

$T_{avg}$  = Avg. temperature of the gas, K (from "Panhandle A Eqn US"sheet)

$Z_{avg}$  = average compressibility factor, dimensionless (from "Panhandle A Eqn US"sheet)

**Inputs**

$P_{avg}$ =	6324.3	kPa (abs)
$T_{avg}$ =	301.89	K
$Z_{avg}$ =	0.88	
MW =	17.38	kg/k-mol
R =	8.314	kPaa*m <sup>3</sup> /kmol-K

**Calculations**

$T_{avgR}$ =	543.40	R
$\rho_{avg}$ =	0.049	g/ml
K =	0.0112	
X =	6.2583	
Y =	1.3603	
$\mu_{avg}$ =	0.0125	cP
	0.000125	P