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Chris Haslego  
President  
Cheresources, Inc.

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1422 Goswick Ridge Road  
Midlothian VA 23114

Fax: 561-658-6489  
Email: [support@cheresources.com](mailto:support@cheresources.com)

***Content Based  
Chemical Engineering***

**FANNING - LIQUID FLOW / FIND FLOW - PSI KNOWN**

**BASIS:** CRANE TECHNICAL PAPER 410 and MARKS' MECHANICAL ENGINEERS HANDBOOK. Friction factors for smooth (PVC, etc) and rough (Cast) pipe are included. PERRY'S CHEMICAL ENGINEERS HANDBOOK used for viscosities.

**NOTE:** Always begin a new case by retrieving the original file. Direct entry of data in cells that originally contain table lookups could cause functions to be lost, or incorrect calculations. I format cells requiring entry colored **RED**; calculated values are black.

- 1.) Enter identification at [B4]
- 2.) Enter the pipe ID at [C7], use [=], then go to pipe table, eg: [=F61] is the ID for 1 1/2" schd 40, or [=G61] metric ( 40 mm ) or directly enter the size if it is not in table.
- 3.) Enter straight length at [C8]
- 4.) Enter pipe material at [C9], use [=], then go to material name in table (A56...A63) eg. [=A56] is Carbon Steel. **NOTE: Typing in a material type can LOCK the program up!**
- 5.) Enter inlet pressure at [B13]
- 6.) Enter outlet pressure at [B14]
- 7.) Enter elevation difference at [B15] (NOTE: Outlet - Inlet)
- 8.) Enter fluid name at [F7], use [=], then go to liquid table. eg. [=D125] is "WATER", or directly enter if not in table.
- 9.) Enter fluid temperature at [F8]
- 10.) If the liquid [F7], is in the liquid table, a representative specific gravity will show at [F9], otherwise directly enter it at [F9]. Check that the sp. gr. value is appropriate for the particular application.
- 11.) If the liquid [F7], is in the liquid table, the viscosity is automatically calculated at its temperature [F8], otherwise directly enter fluid viscosity at [F11]. **Note: no limits are built into viscosity calcs, eg. they will calculate a value for water at 12 deg F. and 450 deg F. If using the calculated viscosity, always check for reasonability, and change of state.**
- 12.) Enter the number of each type of valve & fitting just to their left. [A20]...[A27] & [D20]...[D27]
- 13.) Enter the reducer nominal size, eg: "4/6" or "6/4" (dia1/dia2) at [F29] and [F30] to determine the beta coefficient. The size change 'k' will be calculated and included via [C33] and [C34]. For cases of NO increasers or reducers F29 & F30 should have a ' 0' to zero out C33 & C34.
- 14.) Enter the manufacturer's certified test value of  $K_R$  for the rupture disk in cell [F32], when available. When a disk is included, the calculated flow capacity in cell [E47] is decreased to compensate for the 10% capacity reduction required by the (ASME) Code. The new calculated flow capacity is shown in cell [E51].
- 15.) If a manufacturer's certified test value is not available use the (ASME Code) default value of 2.4.
- 16.) Misc items: for any item where `K' is not known but an equivalent length is, enter the value at [F33].
- 17.) Entrance and exit losses: normally 0.5 and 1.0, are entered at [C31] and [C32] as desired.
- 18.) Misc K: for any item where `K' is known, but not listed above. Enter value at [C35]. Note: to calculate `K' for control valve, or equivalent `K' for line size change, see [A66] thru [B90].
- 19.) Additional delta P if pressure drop is known can be added at [F35].
- 20.) Push the CALCULATE button at [H41] for the iterative calculation to take place and zeroing of the % error.  
Flow `W' is calculated and shown at [E47]. Error flags will show at [C52] & [C53], check for conformance before printing out.

**Print out using direct Excel commands. This application is provided by Chemical Engineers Resource Website, visit [cheresources.com](http://cheresources.com) for additional selections.**

**Print out using direct EXCEL commands.**

<<<<<<<< Psafety © January 2001, by Don Coffman >>>>>>>>

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Consistent with GOOD ENGINEERING PRACTICE, the burden rests with the USER of these spreadsheets to review ALL calculations, and assumptions. The USER IS FULLY RESPONSIBLE for the results or decisions based on calculations.

This Spreadsheet Requires MACROS to be ENABLED to ASSURE proper operation. See the Workbook Help Sheet for Additional Instructions on Use.

dmcoffman@aol.com

Fanning - Liquid Flow / Find Flow - psi known

PIPE: Hazard #8; Seal Water Pump; C-975472

..... System .....	..... Fluid .....
pipe ID : 1.61 in	fluid : WATER
length : 20 ft	temp : 100 °F
material : Stainless Steel	sp. gr.: 0.992
	density: 61.918 lb/ft <sup>3</sup>
	visc. : 0.679 μ, cps
<b>..... Pressures .....</b>	
P1 - in : 25 psig	P1 - P2 : 25 psi, gauge pressure delta
P2 - out : 0 psig	P elev : -7.74 psi, loss due to elevation
h2 - h1 : -18 ft	ΔP : 32.74 psi, or 76.1 feet of head

..... Fitting Losses ... fitting friction factor, *f* : 0.021

..... valves .....	..... fittings .....
0 gate valve 0.000	1 thru `T' 0.410
0 globe valve 0.000	1 branch `T' 1.231
0 angle valve 0.000	0 scrwd 90° 0.000
1 ball valve 0.062	0 scrwd 45° 0.000
0 plug valve 0.000	0 short 90° 0.000
0 diaph valve 0.000	0 short 45° 0.000
0 b'fly valve 0.000	5 long 90° 1.436
1 swing check 1.026	0 long 45° 0.000
 	<b>..... size change .....</b>
valves total : 1.088	reducer 0.000 dia. <sub>1</sub> / dia. <sub>2</sub>
fittings total : 3.078	increaser 0.000 dia. <sub>1</sub> / dia. <sub>2</sub>
entrance : 0.500	
exit : 1.000	rupture disk : 0.0 K <sub>R</sub>
reducer, K : 0.000	misc items equiv len : 0.0 feet
increaser, K : 0.000	final length, l' : 20.0 feet
misc. K : 0.000	add'l equip. ΔP : 0 psig
<hr style="width: 50%; margin-left: 0;"/>	
ΣK: 5.665	

assum *f* = 0.02082      calculated *f* = 0.02082      error *f* = 0.00%

12 · <i>f</i> · l'/d : 3.104	6.3 · (W/dz) : 429797 Re
N : 8.769	velocity : 23.7 fps

..... Flow .....

$$W := \sqrt{\frac{(\Delta P - \text{elev}_{\text{loss}}) \cdot D \cdot d^4}{(2.79 + 10^{-7}) \cdot \frac{12 \cdot f \cdot l}{d} + \Sigma K}} = 74,618 \text{ lb/hr, or } 150 \text{ gpm}$$

Fanning - Liquid Flow / Find Flow - psi known
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PIPE: WATER SUPPLY PUMP TO STORAGE

..... System .....	..... Fluid .....
pipe ID : 108.2 millimeter	fluid : WATER
length : 6.096 meter	temp : 37.7778 °C
material : Stainless Steel	sp. gr.: 1.000
	density: 1000 kg/m <sup>3</sup>
	visc. : 0.0006794 z, Pa sec
<b>..... Pressures .....</b>	
P1 - in : 1450 Pa	P1 - P2 : 1450 Pa, gauge pressure delta
P2 - out : 0 Pa	P elev : 0.00 Pa, loss due to elevation
h2 - h1 : 0 meter	ΔP : 1450.00 Pa, or 0.1 meter of head

..... **Fitting Losses** ... fitting friction factor, *f*<sub>t</sub> : 0.017

..... valves .....	..... fittings .....	..... size change .....
0 gate valve 0.000	1 thru `T' 0.333	reducer 0.000 dia. <sub>1</sub> / dia. <sub>2</sub>
0 globe valve 0.000	1 branch `T' 1.000	increaser 0.000 dia. <sub>1</sub> / dia. <sub>2</sub>
0 angle valve 0.000	0 scrwd 90° 0.000	rupture disk : 0.0 K <sub>R</sub>
1 ball valve 0.050	0 scrwd 45° 0.000	misc items equiv len : 0.0 meter
0 plug valve 0.000	0 short 90° 0.000	final length, l' : 6.1 meter
0 diaph valve 0.000	0 short 45° 0.000	add'l equip. ΔP : 0 Pa
0 b'fly valve 0.000	5 long 90° 1.167	
1 swing check 0.834	0 long 45° 0.000	
valves total : 0.884		
fittings total : 2.501		
entrance : 0.500		
exit : 1.000		
reducer, K : 0.000		
increaser, K : 0.000		
misc. K : 0.000		
ΣK: 4.884		

assum *f* = 0.022388      calculated *f* = 0.022387      error *f* = 0.00%

f · l/d : 1.261	1.27 · (W/dz) : 109,302 Re	
N : 6.146	velocity : 0.69 mps	

..... **Flow** .....

$$W := \sqrt{\frac{(\Delta P - \text{elev loss}) \cdot D \cdot d^4}{(808 \cdot 10^{-3}) \cdot \frac{f \cdot l}{d} + \Sigma K}} = 6.32624081 \text{ kg/sec, or } 22.774467 \text{ m}^3/\text{hr}$$

material table		PIPE				COPPER TUBING				Sanitary Tubing			
material	epsilon	inside diameter				inside diameter				Nominal	Inside	Wall	Outside
		nominal diameter	schd 10S	schd 40	schd 80	nominal diameter	Type K	Type L	Type M	Size	Diameter	Thickness	Diameter
Carbon Steel	150	1/2	0.674	0.622	0.546	1/8	0.186	0.200	0.200	1/4	0.180	0.035	0.25
Cast Iron	850	3/4	0.884	0.824	0.742	1/4	0.311	0.315	0.325	3/8	0.305	0.035	0.38
CU tubing	5	1	1.097	1.049	0.957	3/8	0.402	0.430	0.450	1/2	0.370	0.065	0.50
glass	5	1 1/4	1.422	1.380	1.278	1/2	0.527	0.545	0.569	3/4	0.620	0.065	0.75
kynar	5	1 1/2	1.682	1.610	1.500	5/8	0.652	0.666	0.690	1	0.870	0.065	1.00
PVC	5	2	2.157	2.067	1.939	3/4	0.745	0.785	0.811	1 1/2	1.370	0.065	1.50
SS tubing	5	2 1/2	2.635	2.469	2.323	1	0.995	1.025	1.055	2	1.870	0.065	2.00
Stainless Steel	150	3	3.260	3.068	2.900	1 1/4	1.245	1.265	1.291	2 1/2	2.370	0.065	2.50
		3 1/2	3.760	3.548	3.364	1 1/2	1.481	1.505	1.571	3	2.834	0.083	3.00
		4	4.260	4.026	3.826	2	1.959	1.985	2.009	4	3.834	0.083	4.00
		6	6.357	6.065	5.761	2 1/2	2.435	2.465	2.495	6	5.782	0.109	6.00
		8	8.329	7.981	7.625	3	2.907	2.945	2.981	8	7.782	0.109	8.00
		10	10.420	10.020	9.562	3 1/2	3.385	3.425	3.459				
		12	12.390	11.938	11.374	4	3.857	3.905	3.935				
		14	13.624	13.124	12.500	5	4.805	4.875	4.907				
		16	15.624	15.000	14.312	6	5.741	5.845	5.881				
		18	17.624	16.867	16.124	8	7.583	7.725	7.785				
		20	19.564	18.812	17.938								
		24	23.500	22.624	21.562								

  

for control valve:

$C_v = 25.6$

$K = \frac{891d^4}{C_v^2}$

$K = 9.135$

size change, equivalent K:

convert diameter

$d' = 1.610$

with resistance of

$K' = 3.80$

in terms of

$d = 1.610$

$\beta = d'/d = 1.000$

$K_1 = \frac{K}{\beta^4} = 3.80$

orifice equivalent length:

$K_o = 0.60$

$A = 1.00$

$l = \frac{0.05d^5}{K_o^2 A^2 i}$

$l = 73.6$  eq. feet

liquid	visc (cp)	spec. grav	Pipe Friction Data - Crane TP-410		
			Nominal Size	Friction Factor, ft	Next Pipe Size
ACETIC ACID 100%	0.986	1.050	0.200	0.0373	0.300
ACETIC ACID 70%	1.820	1.010	0.300	0.0327	0.400
ACETONE	0.267	0.789	0.400	0.0300	0.500
AMMONIA 26%	0.814	0.905	0.500	0.0281	0.750
AMMONIA 100%	0.082	0.682	0.750	0.0250	1.000
BENZENE	0.514	0.844	1.000	0.0231	1.500
BLACK LIQUOR 50%	67.828	1.250	1.500	0.0208	2.000
BLACK LIQUOR 63%	1186.796	1.330	2.000	0.0194	2.500
BLACK LIQUOR 68%	6319.631	1.360	2.500	0.0184	3.000
BRINE, CALCIUM CHLORIDE 25%	1.328	1.230	3.000	0.0177	3.500
BRINE, SODIUM CHLORIDE 25%	1.301	1.190	3.500	0.0170	4.000
CARBON DIOXIDE	0.063	1.102	4.000	0.0165	5.000
CAUSTIC 20%	2.679	1.223	5.000	0.0157	6.000
CAUSTIC 50%	39.945	1.530	6.000	0.0151	8.000
CHLORINE LIQUID	0.317	1.467	8.000	0.0142	10.000
CONDENSATE	0.680	0.996	10.000	0.0136	12.000
DOWTHERM A	2.930	0.995	12.000	0.0131	14.000
ETHANOL 100%	0.762	0.789	14.000	0.0127	16.000
ETHANOL 40%	1.418	0.935	16.000	0.0124	20.000
ETHANOL 95%	0.905	0.804	20.000	0.0119	24.000
ETHYL CHLORIDE	0.234	0.923	24.000	0.0115	36.000
ETHYLENE GLYCOL	11.374	1.110	36.000	0.0107	48.000
FREON, R11	0.389	1.410	48.000	0.0101	60.000
FREON, R12	0.245	1.170			
FREON, R22	0.208	1.440			
FUEL OIL #2	2.799	0.876			
FUEL OIL #6	185.462	0.993			
GASOLINE	0.511	0.751			
GLYCEROL, 100%	376.300	1.260			
HYDROCHLORIC 31.5%	1.556	1.159			
ISOPROPYL ALCOHOL	1.257	0.785			
KEROSENE	1.491	0.811			
LUBE OIL MOBIL 634	420.342	0.884			
METHANOL 100%	0.453	0.796			
METHANOL 40%	1.556	0.937			
METHANOL 90%	0.586	0.824			
METHYL CHLORIDE	0.229	0.998			
MULTITHERM PG-1	23.148	0.875			
NITRIC ACID 60%	1.729	1.370			
NITRIC ACID 95%	0.872	1.500			
OIL, VEGETABLE HARDENED	45.541	0.920			
OIL, VEGETABLE UNHARDENED	34.966	0.880			
SULPHUR DIOXIDE	0.294	1.434			
SULPHURIC 110%, FUMING	27.430	1.840			
SULPHURIC ACID 60%	4.419	1.500			
SULPHURIC ACID 98%	13.918	1.830			
TOLUENE	0.493	0.862			
TURPENTINE	1.041	0.864			
WATER	0.679	0.992			

  

Factor, ft Interpolation		
1.50	0.0208	
1.610	0.0205	
2.00	0.0194	